



Project QUARTET has received funding from the European Unions Horizon 2020 research and innovation programme under grant agreement No 862644

## Quantum Illumination Radars: Relaxed Assumptions and Limitations

Reference: A. Karsa, G. Spedalieri, Q. Zhuang, & SP, *Quantum Illumination with a generic Gaussian source*,

Phys. Rev. Research 2, 023414 (2020)

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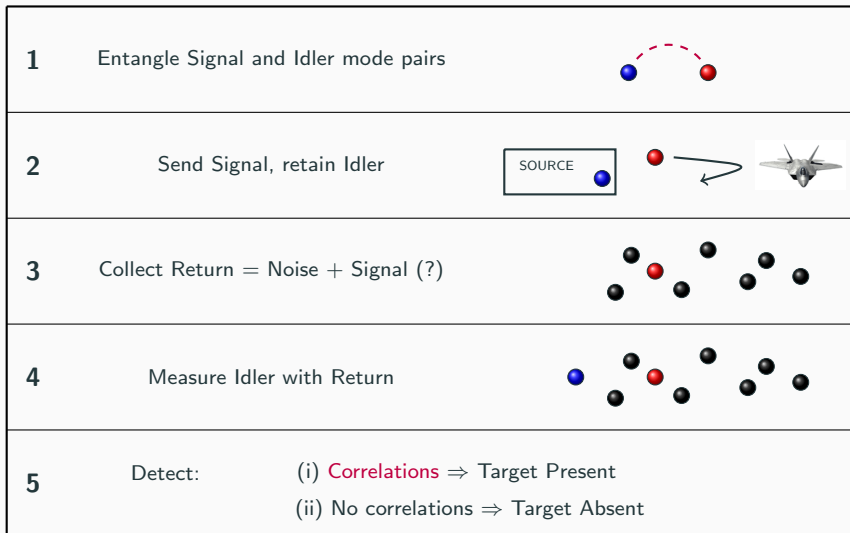
Stefano Pirandola

15-16 July 2020

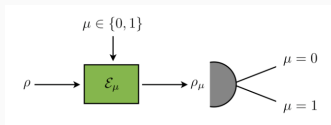
Quantum Radar Workshop, Applied Research Laboratory for Intelligence and Security (ARLIS)  
University of Maryland, College Park, Maryland, USA

- Review on photonic quantum sensing covering the protocol of Gaussian quantum illumination (optical/microwave):
- **Advances in photonic quantum sensing**  
S. Pirandola, B.R. Bardhan, T. Gehring, C. Weedbrook, S. Lloyd  
Nature Photonics 12, 724-733 (2018)
- Has discussion on challenges and limits of quantum lidar/radar.

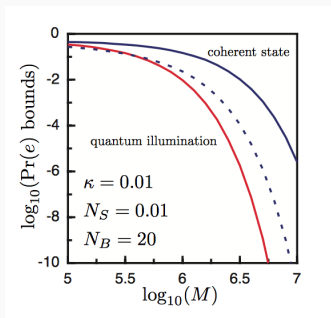
# Basic QI protocol



# Quantum hypothesis testing



- Quantum radar detection can be modelled as a problem of binary QHT: task reduced to distinguishing output states  $\rho_\mu$ .
- Requires  $\rho_\mu^{\otimes M}$  with  $M \gg 1$



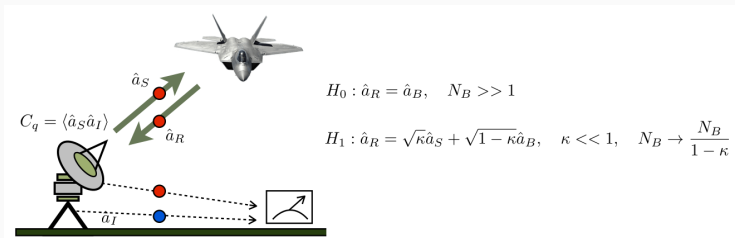
$$P_{\text{err}}^{QI} = \frac{1}{2} \exp\left(-\frac{M\kappa N_S}{N_B}\right) \quad (1)$$

$$P_{\text{err}}^{CS} = \frac{1}{2} \exp\left(-\frac{M\kappa N_S}{4N_B}\right) \quad (2)$$

## What we do...

- Generalise the definition of a quantum radar beyond QI:  
*Any model that exploits a quantum part or device to outperform a corresponding classical radar under the same conditions of energy, range, etc.*
- We progressively relax entanglement requirements of QI and study the corresponding detection performances to the point where the source becomes just-separable, i.e., a maximally-correlated separable state.
- At the same time, try to formulate equivalences between figures of merit between classical and quantum radar performance.

# General quantum-correlated source



We consider a source modelled as a two-mode Gaussian state:

$$\mathbf{v}_{SI}^{gen} = \begin{pmatrix} S & C \\ C & S \end{pmatrix} \oplus \begin{pmatrix} S & -C \\ -C & S \end{pmatrix}, \quad (3)$$

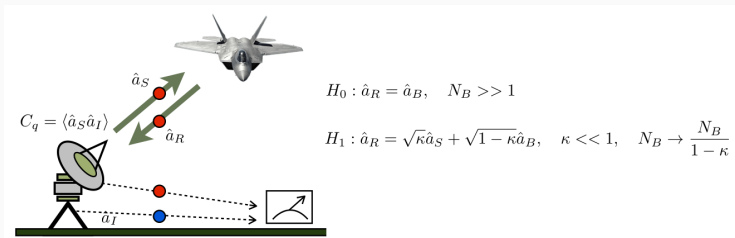
where

$$S := N_S + 1/2,$$

$$0 \leq C \leq \sqrt{S^2 - 1/4} = \sqrt{N_S(N_S + 1)} = C_q,$$

$$C_d = N_S.$$

# General quantum-correlated return



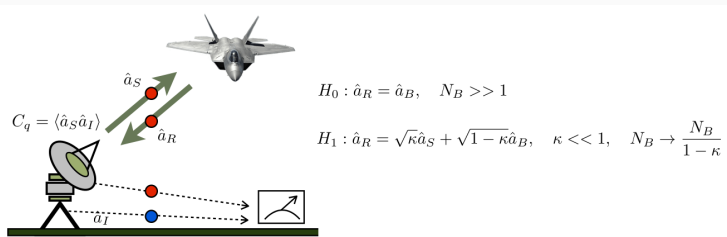
The joint state of our returning ( $R$ ) mode and the retained idler is given by, under  $H_0$  and  $H_1$ , respectively:

$$\mathbf{v}_{RI}^{(0)} = \begin{pmatrix} B & 0 \\ 0 & S \end{pmatrix} \oplus \begin{pmatrix} B & 0 \\ 0 & S \end{pmatrix}, \quad (4)$$

$$\mathbf{v}_{RI}^{(1)} = \begin{pmatrix} A & \sqrt{\kappa}C \\ \sqrt{\kappa}C & S \end{pmatrix} \oplus \begin{pmatrix} A & -\sqrt{\kappa}C \\ -\sqrt{\kappa}C & S \end{pmatrix}, \quad (5)$$

where  $B := N_B + 1/2$  and  $A := \kappa N_S + B$ .

# Coherent state scenario - no access to idler



- Signal mode, annihilation operator  $\hat{a}_S$ , prepared in the coherent state  $|\sqrt{N_S}\rangle$
- $H_0$ : return is in a thermal state with mean photons per mode  $N_B$ , mean vector of zero and CM  $(N_B + 1/2)\mathbf{1}_2$ .
- $H_1$ : return corresponds to a displaced thermal state with mean vector  $(\sqrt{2\kappa N_S}, 0)$  and CM  $(N_B + 1/2)\mathbf{1}_2$ .



# Hypothesis testing for quantum radar detection

- Detection probability  $P_d := P(H_1|H_1)$ .
- Two types of error may occur:  
type-I (false-alarm)  $P_{fa} = P(H_1|H_0)$ , and  
type-II (missed detection)  $P_{md} = P(H_0|H_1)$ .
- One may consider *asymmetric* testing in order to take in account discrepancies in error cost.
- A *symmetric* approach aims to obtain a global minimisation over all errors, irrespective of their origin. In this case, one considers the minimization of the average error probability

$$P_{\text{err}} := P(H_0)P(H_1|H_0) + P(H_1)P(H_0|H_1). \quad (6)$$

# Symmetric hypothesis testing

- *Minimum* error probability is given by the Helstrom bound:  
 $P_{\text{err}}^{\min} = [1 - D(\hat{\rho}_0, \hat{\rho}_1)] / 2$ , where  $D(\hat{\rho}_0, \hat{\rho}_1) := |\hat{\rho}_0 - \hat{\rho}_1|/2$  is the trace distance.
- Analytically, use QCB,

$$P_{\text{err}}^{\min} \leq P_{\text{err}}^{\text{QCB}} := \frac{1}{2} \left( \inf_{0 \leq s \leq 1} C_s \right), \quad C_s := (\hat{\rho}_0^s \hat{\rho}_1^{1-s}). \quad (7)$$

- Forgoing minimization, set  $s = 1/2$  and define a simpler, though weaker, upper bound, the QBB

$$P_{\text{err}}^{\text{QBB}} := \frac{1}{2} \left( \sqrt{\hat{\rho}_0} \sqrt{\hat{\rho}_1} \right). \quad (8)$$

- For Gaussian states, closed analytical formulae exist for these!

# Symmetric radar detection

- Assume typical condition of QI:  $\kappa \ll 1$ ,  $N_B \gg 1$ ,  $N_S \ll 1$ .
- For a TMSV state, the minimum error probability satisfies

$$P_{\text{err}}^{\text{TMSV}} \leq e^{-M\kappa N_S/N_B}/2. \quad (9)$$

- Computed using the QBB, exponentially tight in limit of large  $M$ .
- Error-rate exponent has a factor of 4 advantage over the corresponding coherent-state transmitter

$$P_{\text{err}}^{\text{CS}} \leq e^{-M\kappa N_S/4N_B}/2. \quad (10)$$

- Extending Eq. (9) to the error probability for a generic source, we find

$$P_{\text{err}}^{\text{gen}} \leq e^{-M\kappa N_S C^2/N_B C_q^2}/2. \quad (11)$$

## Symmetric radar detection - generic source

- Comparing Eqs. (11) and (10), we see that a quantum-correlated transmitter beats the coherent state transmitter if  $P_{\text{err}}^{\text{gen}} \leq P_{\text{err}}^{\text{CS}}$  which means

$$\frac{C^2}{C_q^2} \geq \frac{1}{4} \Rightarrow C \geq \frac{1}{2} \sqrt{N_S(N_S + 1)}. \quad (12)$$

- Thus, the quadrature correlations required to outperform the semi-classical benchmark is **half** the value of those of a TMSV state.
- The employment of a source at the separable limit is not capable of beating coherent states under symmetric testing.

# Asymmetric hypothesis testing 1

- Consider  $M$  copies  $\hat{\rho}_i^{\otimes M}$  of the state  $\hat{\rho}_i$  encoding bit  $i \in \{0, 1\}$ .
- Binary outcome - two types of error, i.e., the type-I (false alarm) error

$$P_{\text{fa}} := P(H_1|H_0) = (E_1 \hat{\rho}_0^{\otimes M}), \quad (13)$$

and the type-II (missed detection) error

$$P_{\text{md}} := P(H_0|H_1) = (E_0 \hat{\rho}_1^{\otimes M}). \quad (14)$$

- These probabilities are dependent on the number  $M$  of copies and, for  $M \gg 1$ , they both tend to zero, i.e.,

$$P_{\text{fa}} \simeq e^{-\alpha_R M}, \quad P_{\text{md}} \simeq e^{-\beta_R M}, \quad (15)$$

where we define the 'error-exponents' or 'rate limits' as

$$\alpha_R = - \lim_{M \rightarrow +\infty} \frac{1}{M} \ln P_{\text{fa}}, \quad \beta_R = - \lim_{M \rightarrow +\infty} \frac{1}{M} \ln P_{\text{md}}. \quad (16)$$

## Asymmetric hypothesis testing 2

- Place a relatively loose constraint  $P_{\text{fa}} < \epsilon$  on the type-I error, allowing us more freedom to minimize  $P_{\text{md}}$ .
- Quantum Stein's lemma: given this constraint, QRE is the optimal decay rate for the type-II error probability

$$D(\hat{\rho}_0 || \hat{\rho}_1) = [\hat{\rho}_0(\ln \hat{\rho}_0 - \ln \hat{\rho}_1)] \quad (17)$$

- Tracking the type-II error exponent to second order (in  $M$ ) depth, that is to order  $\sqrt{M}$ , allows one to define the QRE variance

$$V(\hat{\rho}_0 || \hat{\rho}_1) = [\hat{\rho}_0(\ln \hat{\rho}_0 - \ln \hat{\rho}_1)^2] - [D(\hat{\rho}_0 || \hat{\rho}_1)]^2. \quad (18)$$

- Optimal type-II error probability, for sample size  $M$ :

$$P_{\text{md}} = \exp \left\{ - \left[ MD(\hat{\rho}_0 || \hat{\rho}_1) + \sqrt{MV(\hat{\rho}_0 || \hat{\rho}_1)} \Phi^{-1}(\epsilon) + \mathcal{O}(\log M) \right] \right\}, \quad (19)$$

where  $\epsilon \in (0, 1)$  bounds  $P_{\text{fa}}$  and  $\Phi(y) := \frac{1}{\sqrt{2\pi}} \int_{-\infty}^y dx \exp(-x^2/2)$ .

## Remarks on Literature

- 1 Asymmetric hypothesis testing: Helstrom's and Holevo's books
  - 2 Second-order expansion: Ke Li, Ann. Statist. 42, 171-189 (2014).
  - 3 Computation of the relative entropy:  
Pirandola, Laurenza, Ottaviani, Banchi,  
Nature Communications 8, 15043 (2017)
  - 4 Computation of the relative entropy variance:  
Wilde, Tomamichel, Lloyd, Berta, PRL 119, 120501 (2017)
- Calculations in items 3 and 4 are based on the Gaussian tools/formulas developed in:  
Banchi, Braunstein, Pirandola, PRL 115, 260501 (2015)

# Asymmetric radar detection

- We evaluate the QRE and QRE-variance to first order in  $N_B$  by taking an asymptotic expansion for large  $N_B$  while keeping  $N_S$  fixed. We obtain

$$D_{\text{gen}} := D\left(\hat{\rho}_{RI}^{(0)} \parallel \hat{\rho}_{RI}^{(1)}\right) = \frac{\kappa C^2}{N_B} \ln\left(1 + \frac{1}{N_S}\right) + \mathcal{O}(N_B^{-2}), \quad (20)$$

$$V_{\text{gen}} := V\left(\hat{\rho}_{RI}^{(0)} \parallel \hat{\rho}_{RI}^{(1)}\right) = \frac{\kappa C^2(2N_S + 1)}{N_B} \ln^2\left(1 + \frac{1}{N_S}\right) + \mathcal{O}(N_B^{-2}). \quad (21)$$

- For coherent states these quantities take the form

$$D_{\text{CS}} := D\left(\hat{\rho}_{\text{CS}}^{(0)} \parallel \hat{\rho}_{\text{CS}}^{(1)}\right) = \kappa N_S \ln\left(1 + \frac{1}{N_B}\right) \simeq \gamma + \mathcal{O}(N_B^{-2}), \quad (22)$$

$$V_{\text{CS}} := V\left(\hat{\rho}_{\text{CS}}^{(0)} \parallel \hat{\rho}_{\text{CS}}^{(1)}\right) = \kappa N_S(2N_B + 1) \ln^2\left(1 + \frac{1}{N_B}\right) \simeq 2\gamma + \mathcal{O}(N_B^{-2}), \quad (23)$$

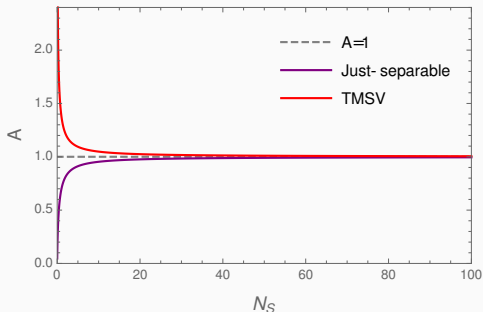
- Signal-to-noise ratio (SNR):  $\gamma := \frac{\kappa N_S}{N_B}$ , usually expressed in decibels (dB) via  $\gamma_{\text{dB}} = 10 \log_{10} \gamma$ .



# Asymmetric performance comparison

Define an error-exponent advantage over coherent states:

$$A(C, N_S) := \frac{D_{\text{gen}}}{D_{\text{CS}}} = \frac{C^2}{N_S} \ln \left( 1 + \frac{1}{N_S} \right). \quad (24)$$



- Benefits of max-entanglement for QI only for very small energies.
- For increasing  $N_S$ , the ratio  $A \rightarrow 1$ , irrespective of source specification.
- Just-separable source quickly approaches the performance of QI already at about 20 photons.

# Receiver operating characteristic

Study mis-detection probability vs false-alarm probability for generic Gaussian source and coherent state classical benchmark.

- Optimal: phase is maintained - homodyne + coherent integration
- Deterministic phase shift - use heterodyne + coherent integration.
- Random phase shift - heterodyne + non-coherent integration, given by **Marcum's Q-function**
- Marcum's Q -function may be overestimated by assuming single coherent pulse with  $MN_S$  photons.

- The ROC  $P_{\text{md}} = P_{\text{md}}(P_{\text{fa}})$  of the gen. quantum source can be upper bounded:

$$P_{\text{md}} \leq \tilde{P}_{\text{md}}^{\text{gen}} = \exp \left\{ - \left[ \sqrt{\frac{M\gamma}{N_S}} \Lambda C \ln \left( 1 + \frac{1}{N_S} \right) + \mathcal{O}(N_B^{-1}, 1) \right] \right\}, \quad (25)$$

$$\Lambda := \left( \sqrt{\frac{M\gamma}{N_S}} C + \sqrt{2N_S + 1} \Phi^{-1}(P_{\text{fa}}) \right). \quad (26)$$

- Sufficiently large  $M$  ( $\gtrsim 10^7$ ) and large  $N_B$  ( $\gtrsim 10^2$ ).

## ROC: coherent states

- Optimal - homodyne + coherent integration and binary testing:

$$P_{\text{CS,hom}}^{\text{fa}}(x) = \frac{1}{2} \operatorname{erfc} \left( \frac{x}{\sqrt{M(2N_B + 1)}} \right), \quad (27)$$

$$P_{\text{CS,hom}}^{\text{md}}(x) = \frac{1}{2} \operatorname{erfc} \left( \frac{M\sqrt{2\kappa N_S} - x}{\sqrt{M(2N_B + 1)}} \right), \quad (28)$$

where  $\operatorname{erfc}(z) := 1 - 2\pi^{-1/2} \int_0^z \exp(-t^2) dt$  is the complementary error function.

- Lower bound to non-coherent integration: assume single coherent state with mean number of photons  $MN_S$  so that the total SNR is given by  $M\gamma$ :

$$P_{\text{md}}^{\text{Marcum}} = 1 - Q \left( \sqrt{2M\gamma}, \sqrt{-2 \ln P_{\text{fa}}} \right), \quad (29)$$

where the Marcum Q-function is defined as

$$Q(x, y) := \int_y^\infty dt te^{-(t^2+x^2)/2} I_0(tx). \quad (30)$$

# Parameters

Focusing on short-range ( $\sim 1\text{m}$ ) applications, e.g. security or biomedical:

- For  $\nu = 1\text{GHz}$  (L band) and  $T = 290\text{K}$  (room temperature), we get  $N_B \simeq 6 \times 10^3$  photons (bright noise)
- Assume broadband pulses, with 10% bandwidth (100MHz), so that their individual duration  $\sim 10\text{ns}$ . Using  $M = 10^8$  pulses then we have an integration time  $\sim 1\text{s}$  - acceptable for slow-moving/still objects.
- Low-energy applications - assume  $N_S = 1$  mean photon per pulse.
- What about the SNR  $\gamma$ ? - Related to overall reflectivity  $\kappa$ , estimated by the radar equation.

# Parameters

- The radar equation relates returning signal power  $P_R$  to the transmitted signal power  $P_T$ :

$$P_R = \frac{GF^4 A_R \sigma}{(4\pi)^2 R^4} P_T \quad (31)$$

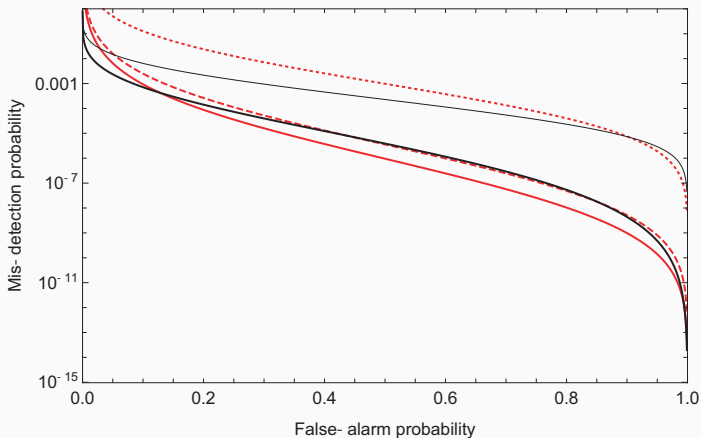
- At the same time, we can also write  $\kappa$  as the ratio:

$$\kappa = \frac{P_R}{P_T} = \frac{GF^4 A_R \sigma}{(4\pi)^2 R^4}, \quad (32)$$

- Assume  $F = 1$  (no free-space loss) and ideal pencil beam so that solid angle  $\delta$  is exactly subtended by the target's  $\sigma$  (valid at short range) so that  $G = 4\pi/\delta = 4\pi R^2/\sigma$ .
- Then,

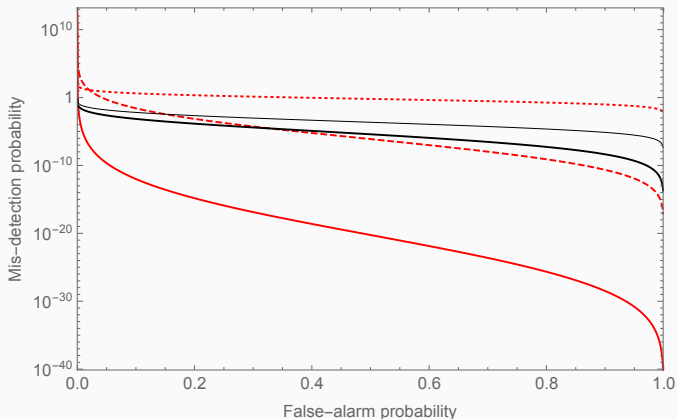
$$\kappa = \frac{A_R}{(4\pi R)^2}, \quad R = \frac{1}{4\pi} \sqrt{\frac{A_R}{\kappa}}. \quad (33)$$

## ROC comparison: $N_S = 1, R = 1m$



- Red curves: Gaussian state QI with  $C(\rho) = pC_d + (1-p)C_q$ . Just-separable,  $p = 0$ , (dotted), maximal entanglement ( $p = 1$ ), solid, and intermediate correlations ( $p = 1/6$ ), dashed.
- Black curves: Classical coherent state benchmark. Optimal homodyne detection, thick, and Marcum bound, thin.

## ROC comparison: $N_S = 0.01, R = 0.1m$



- Red curves: Gaussian state QI with  $C(p) = pC_d + (1-p)C_q$ . Just-separable,  $p = 0$ , (dotted), maximal entanglement ( $p = 1$ ), solid, and intermediate correlations ( $p = 1/2$ ), dashed.
- Black curves: Classical coherent state benchmark  
Optimal homodyne detection, thick, and Marcum bound, thin.



## Concluding remarks

- We have investigated how to loosen QI transmitter requirements.
- Scenarios of symmetric and asymmetric testing where we test the quantum performance with respect to suitable classical benchmarks.
- Quantum advantage still exists by using Gaussian sources which are not necessarily maximally entangled.
- Short ranges only (so spherical beam spreading does not involve too many dBs of loss, a major killing factor for any quantum radar design based on the exploitation of quantum correlations)
- A short-range, low-power radar is potentially interesting as noninvasive scanning tool for biomedical applications but also for short-range security and safety purposes.